

# Progress Toward a Full Uncertainty Propagation Machinery for EDGES

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# Description

This report describes the progress toward a full uncertainty propagation procedure for EDGES.

The procedure is based on a brute-force Monte Carlo, in which the calibration of the antenna temperature is done using calibration quantities modeled using parameter values drawn randomly from distributions derived from their covariance matrices. Figure 1 presents a block diagram of the process.

First, it is necessary to produce an Uncalibrated antenna temperature. This is done using:

- ▶ A sky-beam convolution using the GSM and a flat beam of the form  $\cos^2 \theta$ . The quietest portion is chosen ( $LST \sim 7$ ), and modeled as  $\log(T_{ant}) = \sum_j a_j [\log(\nu/\nu_n)]^j$ . See Figure 2.
- ▶ An antenna S11, with flat magnitude at  $-15$  dB, and with a realistic phase. See Figure 3.
- ▶ The LNA S11 corresponding to a model fit to lab measurements.
- ▶ Scale, offset, and noise wave parameters (nwp) derived from lab measurements: spectra and S11 of Ambient Load, Hot Load, and Open Cable. The modeling of these quantities was done either in terms of polynomials or Fourier series.

The antenna temperature is then *recovered*, using:

- ▶ The perfectly known antenna S11.
- ▶ the LNA S11, whose model parameters are allowed to vary within their covariance.
- ▶ the Scale, Offset, and nwp, recomputed from models of lab measurements allowed to vary within their covariance.

# Description

The sources of uncertainty are:

- ▶ Physical temperature of Ambient Load, Hot Load, and Open Cable. The  $1\sigma$  uncertainty assigned is 0.3 K.
- ▶ Parameter covariance in the model fit to the spectra of the Ambient Load, Hot Load, and Open Cable. This uncertainty depends on the amount of integration of spectra. The results reported here correspond to the integrations conducted at ASU during the receiver calibration.
- ▶ Parameter covariance in the model fit to the Magnitude and Phase of the S11 of the LNA, Ambient Load, Hot Load, and Open Cable. Also, the S12 of the semi-rigid (SR) cable inside the Hot load. This uncertainty depends on the amount of integration of traces. The results reported here correspond to the measurements conducted at ASU during the receiver calibration.
- ▶ Uncertainty in S11 (and S12 for the SR cable of the Hot Load) of 0.01-dB (at  $-20$  dB) and  $0.1^\circ$ , in both cases  $1\sigma$ . The frequency shape of this uncertainty is modeled as a 5-term polynomial, for the magnitude and phase.

# Results

Starting with Figure 4, the effect of each source of uncertainty is observed independently. The blue lines correspond to  $1\sigma$  bounds obtained after running the MC 2000 times. The upper plots correspond to the uncertainty remaining after removing the *perfectly known* input antenna temperature, from the calibrated antenna temperature. The lower plots correspond to the uncertainty after removing the best-fit model of the form  $\log(T_{ant}) = \sum_j a_j [\log(\nu/\nu_n)]^j$ .

In particular, the S11 plots also have a label STAT or SYST, to distinguish between those two cases. The STAT case corresponds to the limitations of modeling the data itself, while SYST accounts for the suspected limitations in the measurement process.

Finally, Figure 30 presents the combined effects, after running the MC 50,000 times. The blue curves represent the effect of all the uncertainties being present simultaneously. The red curves represent the effect of only the systematic uncertainties, i.e., in the physical temperature of the Ambient Load, Hot Load, and Open Cable, and in all the S11 and S12 quantities. Clearly, the uncertainties regarded as systematic are limiting the precision of EDGES. Increasing the integration times used for measurements of spectra and S11 during receiver calibration would not provide significant benefits.

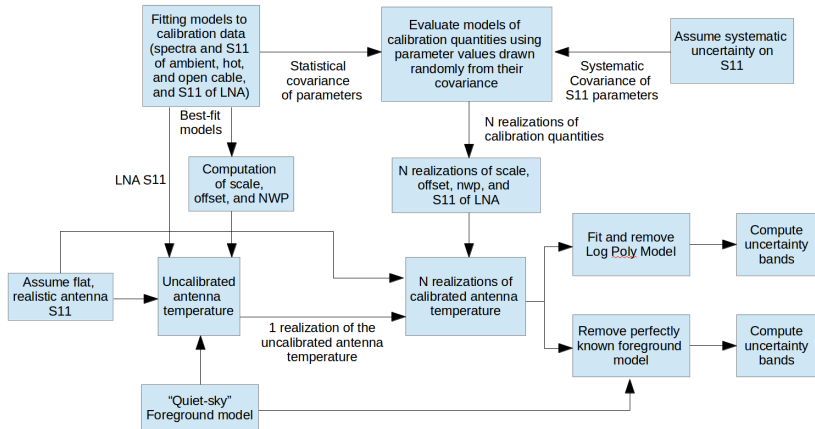


Figure : (1)

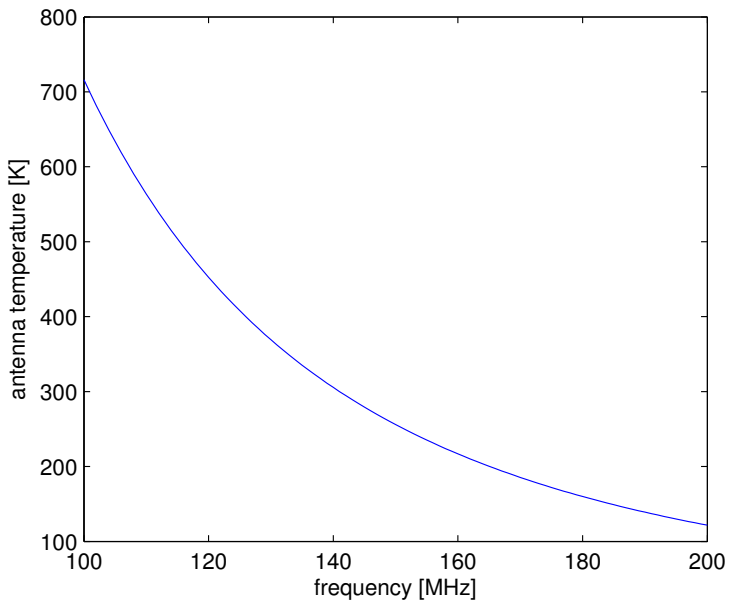


Figure : (2)

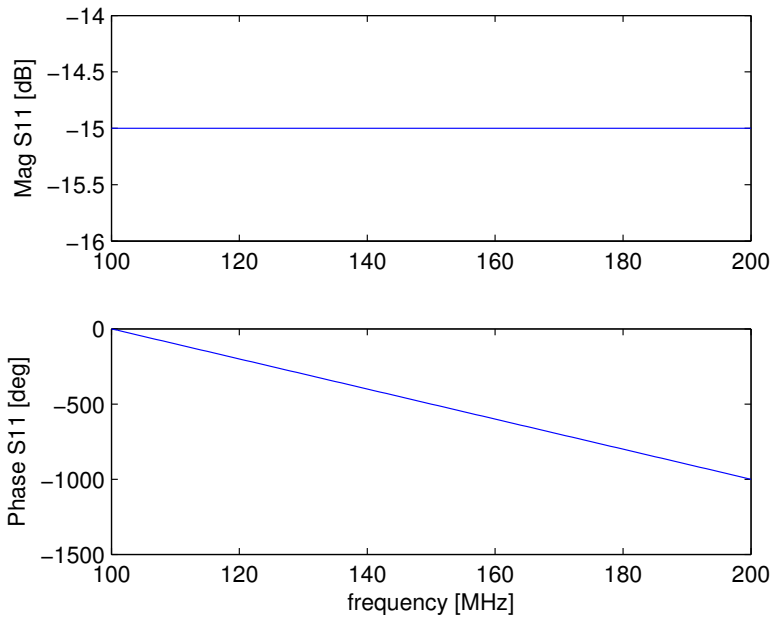


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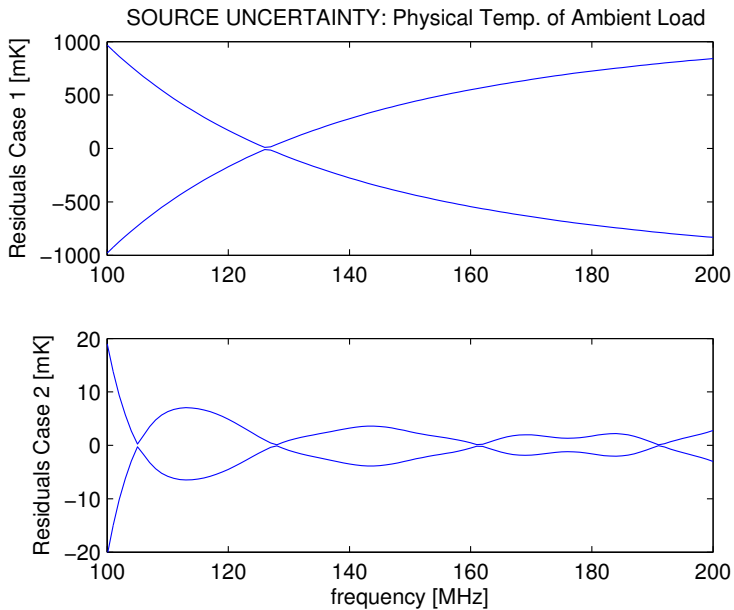


Figure : (4)



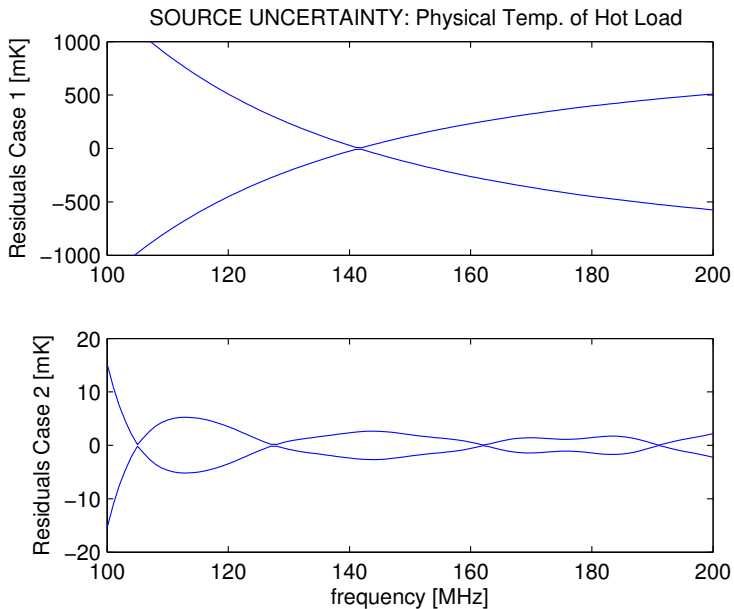


Figure : (5)

### SOURCE UNCERTAINTY: Physical Temp. of Open Cable

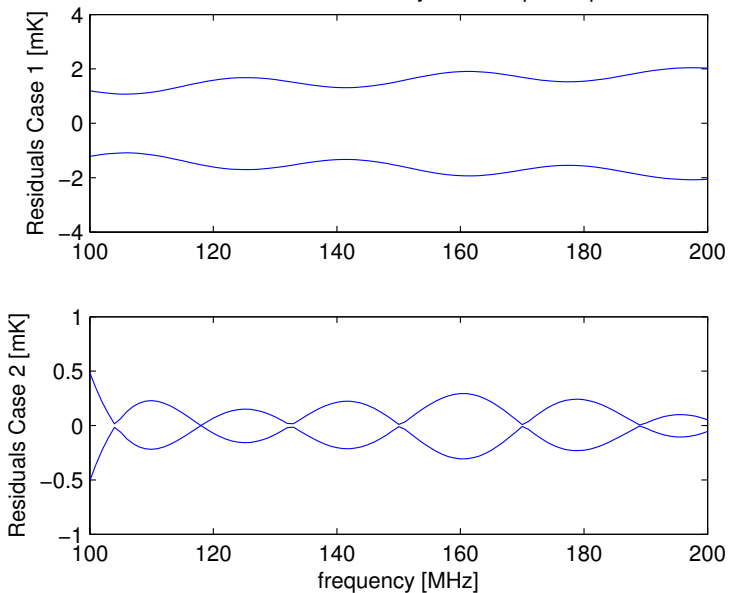


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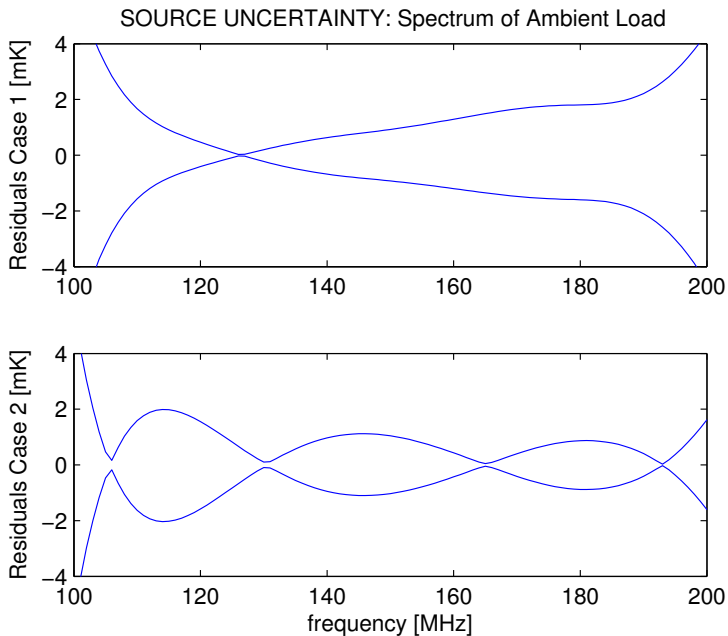


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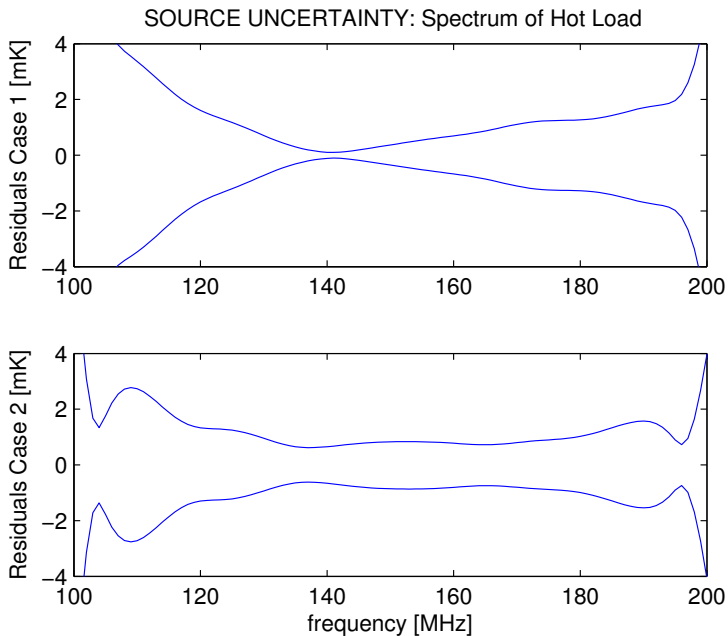


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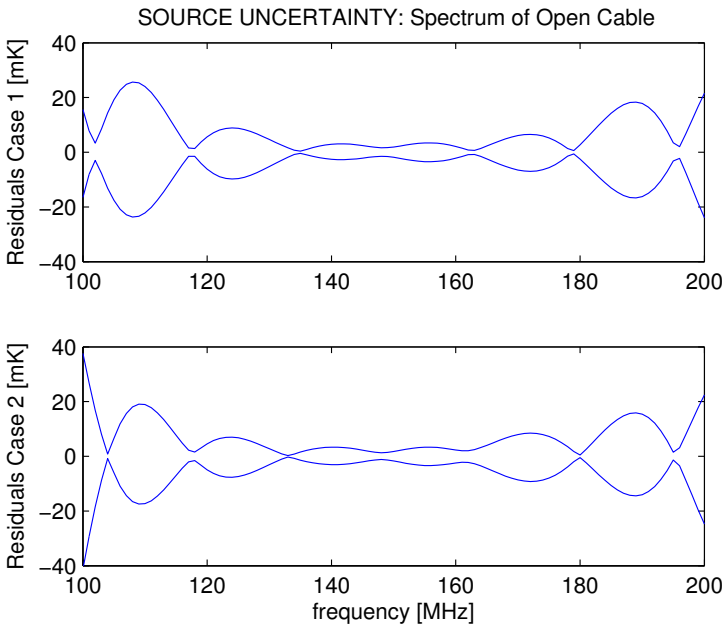


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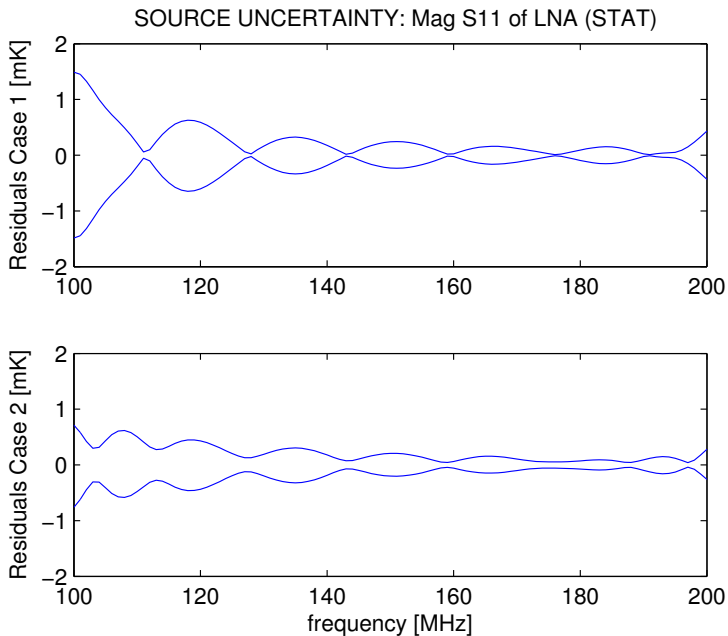


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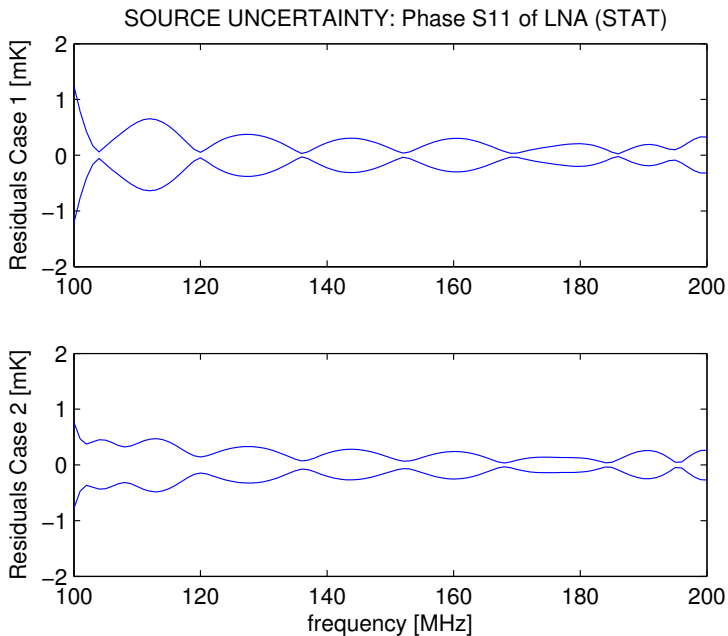


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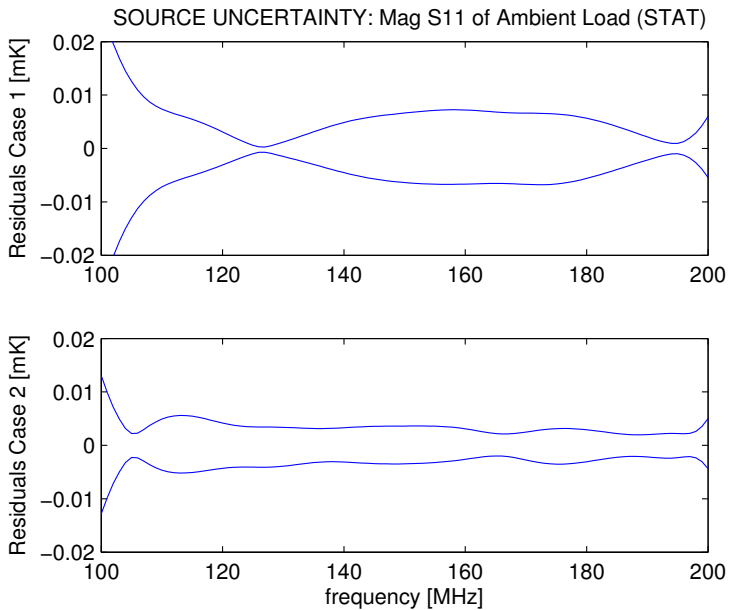


Figure : (12)



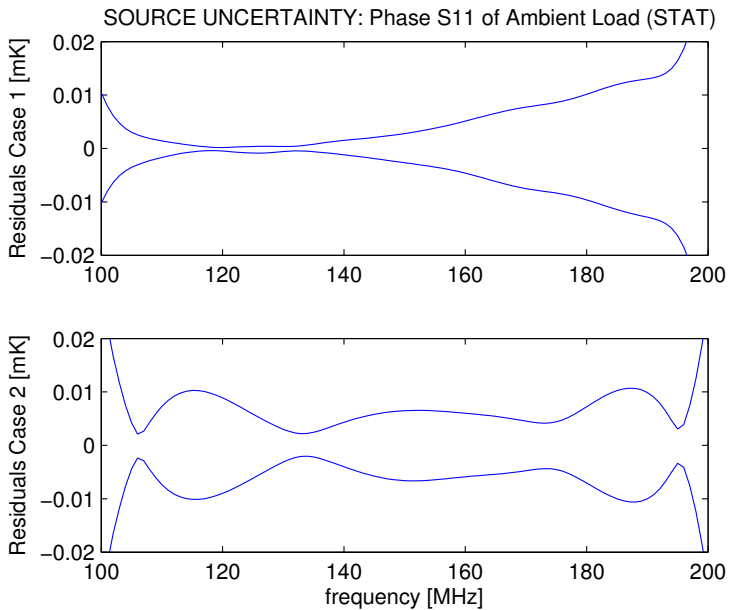


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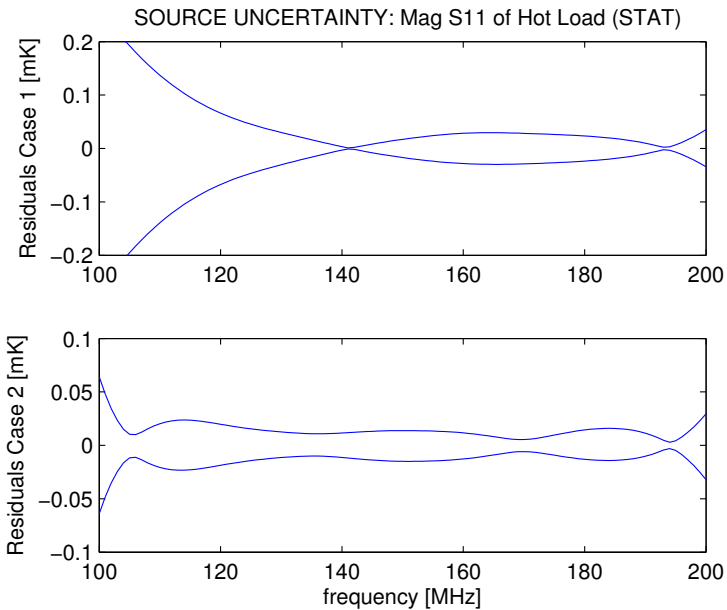


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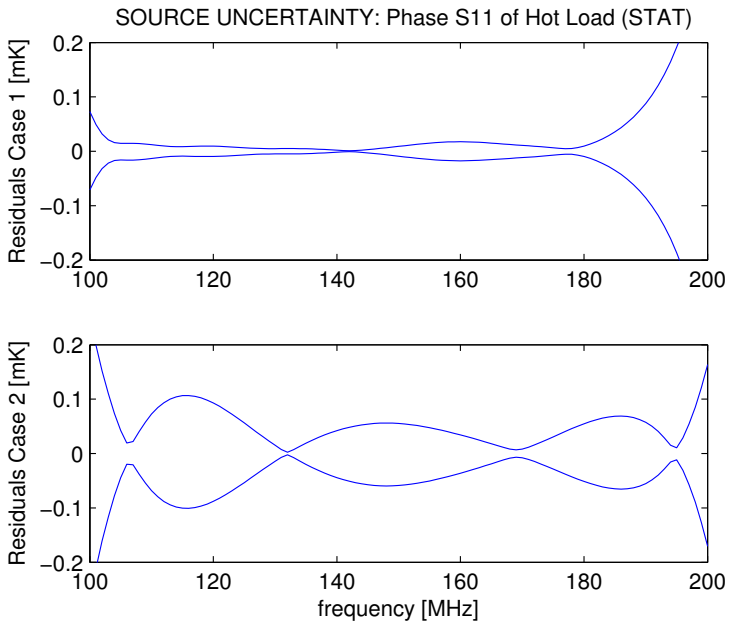


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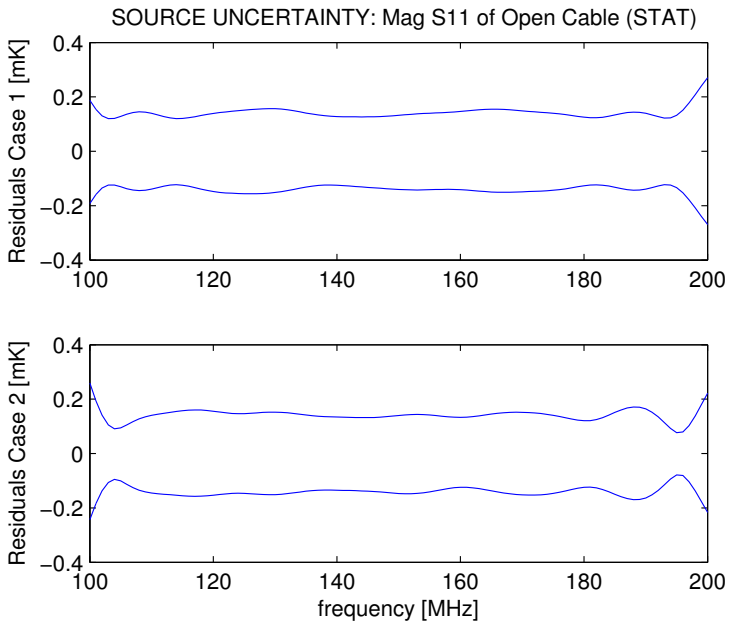


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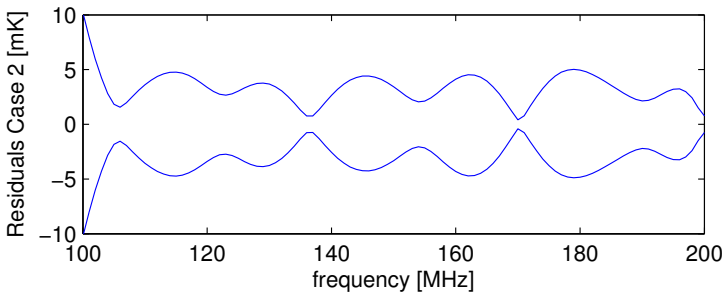
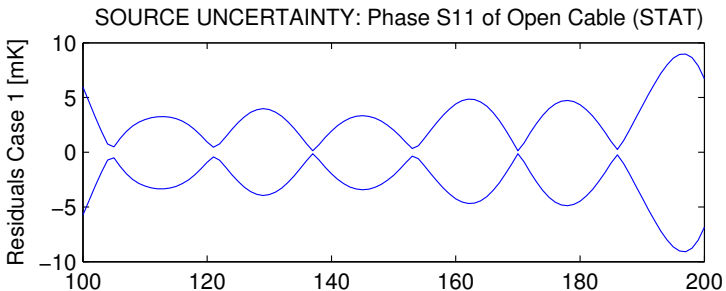


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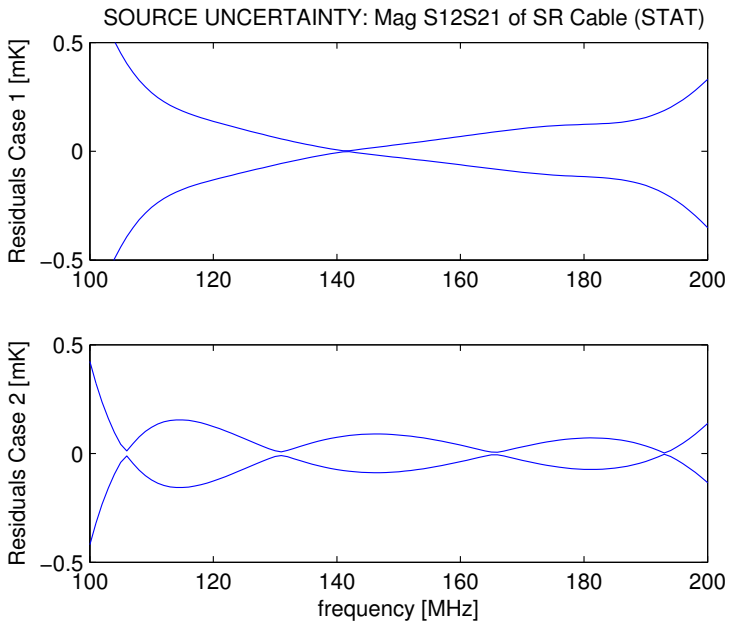


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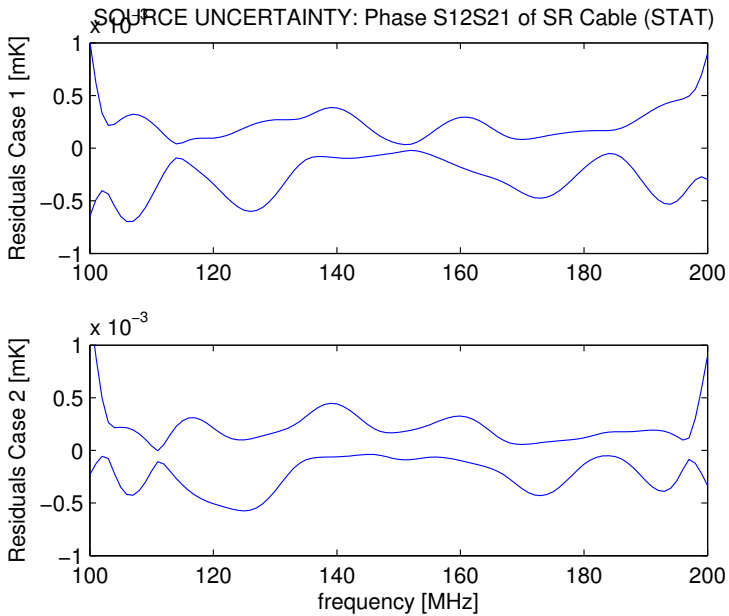


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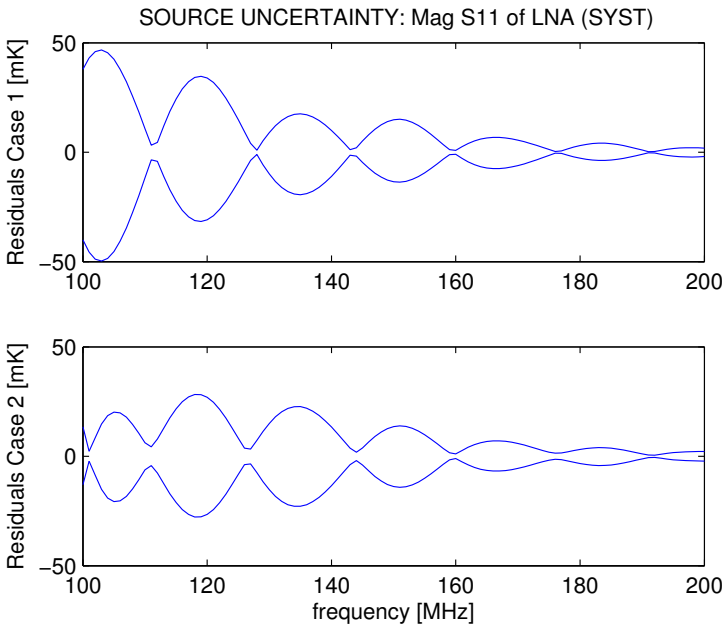


Figure : (20)



### SOURCE UNCERTAINTY: Phase S11 of LNA (SYST)

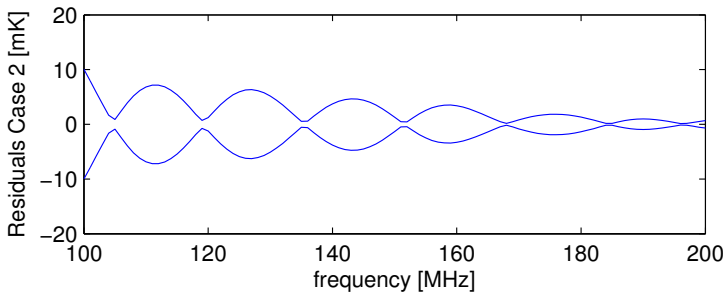
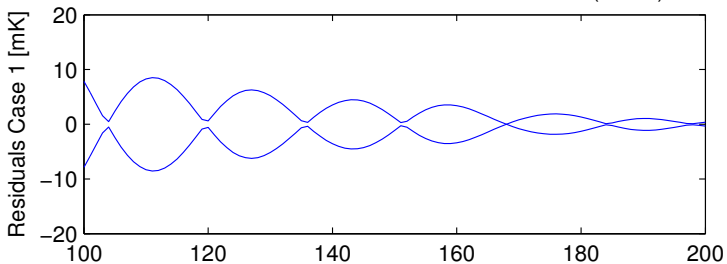


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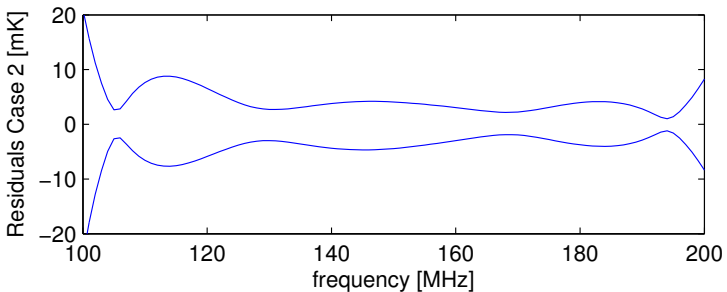
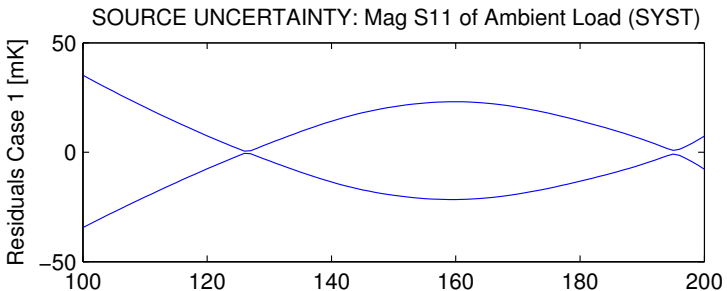


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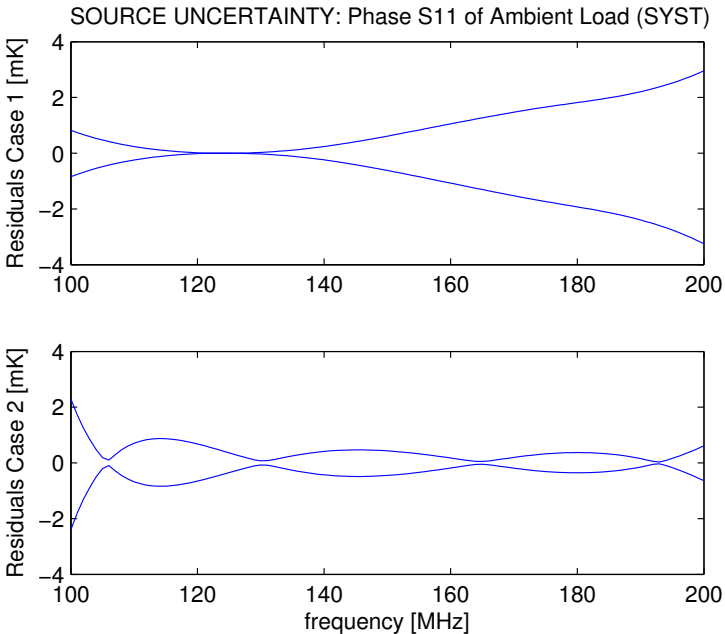


Figure : (23)

SOURCE UNCERTAINTY: Mag S11 of Hot Load (SYST)

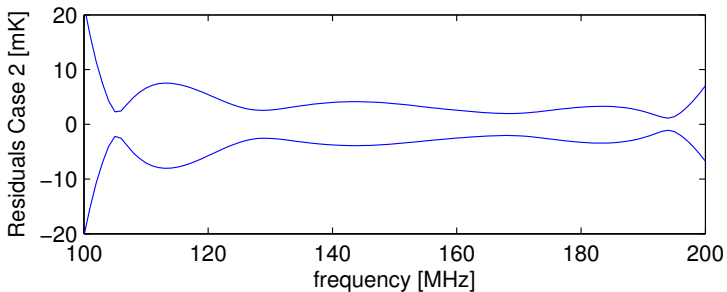
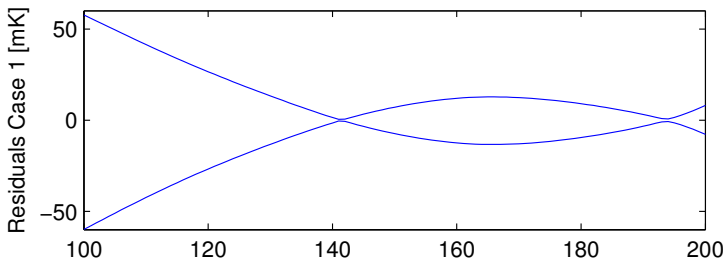


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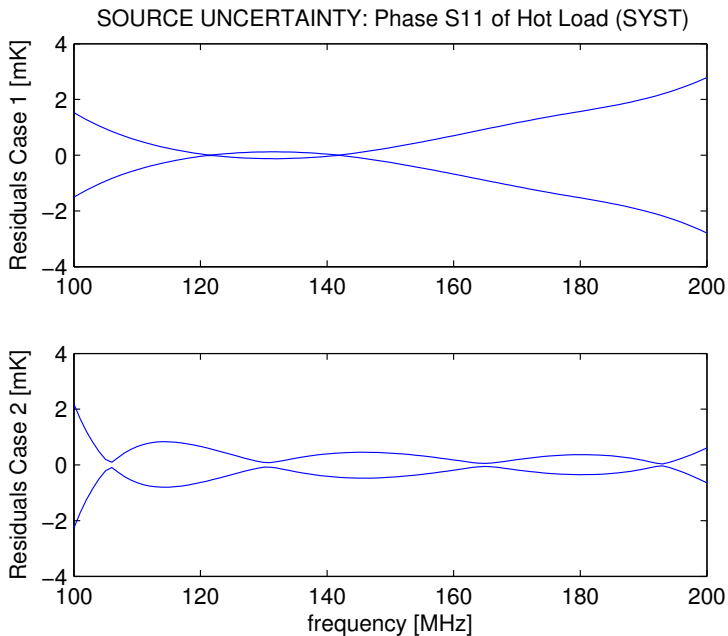


Figure : (25)

### SOURCE UNCERTAINTY: Mag S11 of Open Cable (SYST)

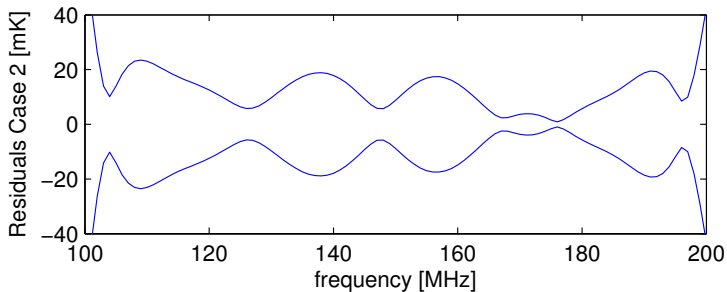
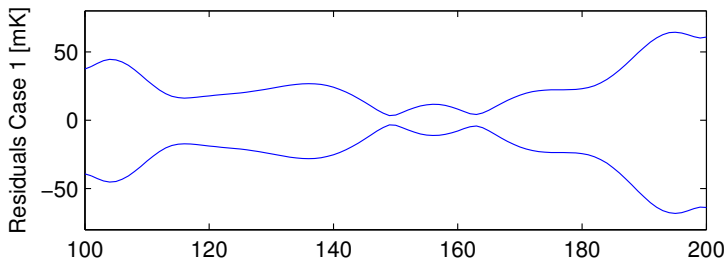


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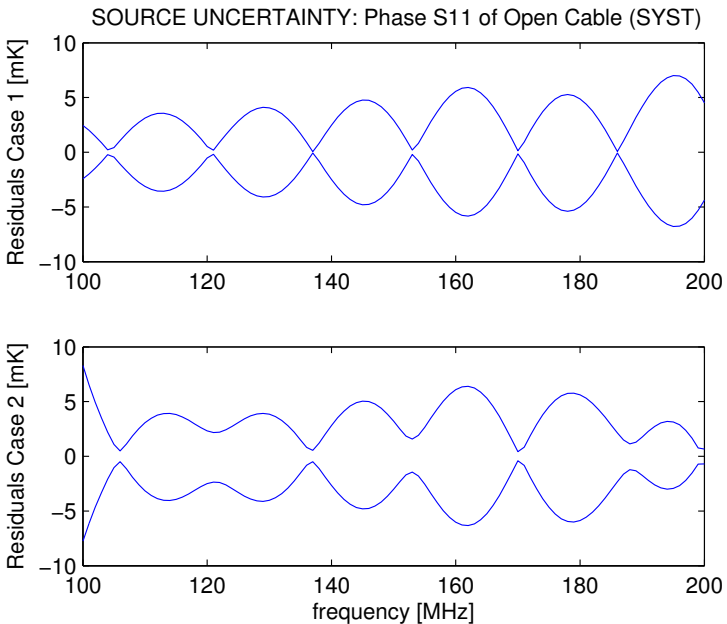


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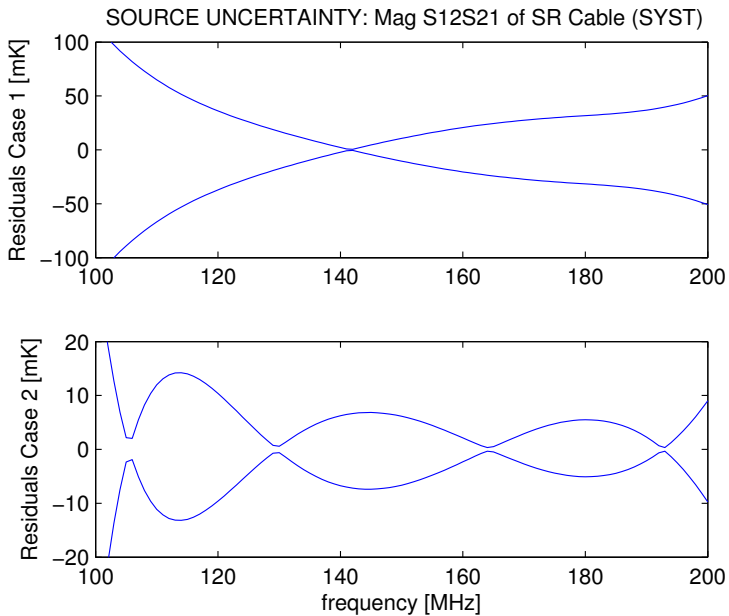


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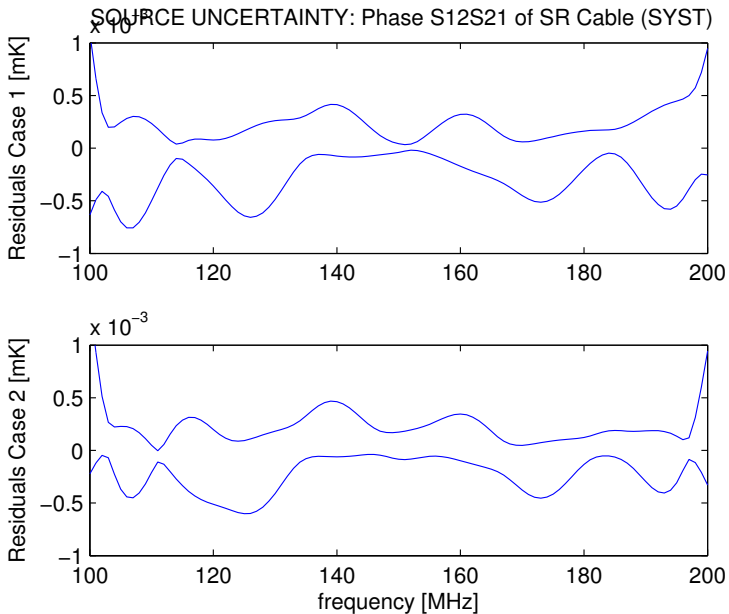


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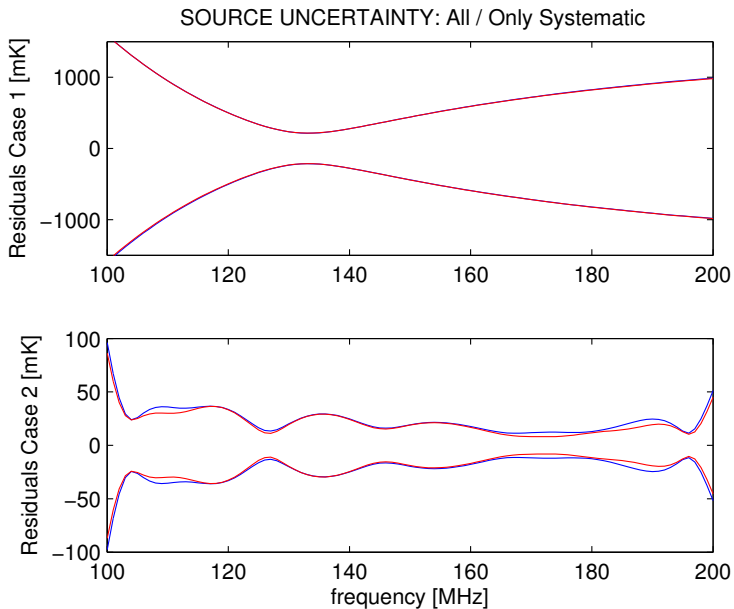


Figure : (30)